

Integrating Particle Swarm Optimization with Analytical Nonlinear Model Predictive Control for Nonlinear Hybrid Systems

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Keywords: Hybrid Systems, Nonlinear Model Predictive Control, Particle Swarm Optimization.

Abstract: The computation load remains the main challenge facing the control techniques of hybrid systems with discrete and continuous control signals. In this paper, a new hybrid controller based on Analytical Nonlinear Model Predictive Control (ANMPC) and Particle Swarm Optimization (PSO) for nonlinear hybrid systems is presented. The proposed controller offer sub-optimal solution in reasonable time while respecting the given constraints. The new developed technique is not considered as a computation burden, thus real-time implementation is possible for many hybrid systems. Besides, it can be applied directly to the nonlinear models, avoiding linearization which may lead to inaccurate model and unexpected behaviour. An application of the proposed controller to a three tanks example is presented.

1 INTRODUCTION

Many real systems can be modelled as hybrid systems with discrete and continuous input signals. Several control techniques have been proposed in literature to control hybrid systems, among them Model Predictive Control (MPC) has been considered as one of the most effective techniques that can control linear hybrid systems. However the computation burden associated with the mixed integer linear/quadratic optimization problems remains the main challenge facing real-time application. Several techniques and algorithms have been proposed in literature to reduce the computation load; for example (Thomas *et al.*, 2003, 2004) proposed using multi-MLD models rather than using one global Mixed Logical Dynamical (MLD) (Bemporad and Morari, 1999) model with bigger number of variables, in (Thomas *et al.*, 2006) a MPC for state partition based MLD model is proposed to use simpler models. A techniques based on genetic algorithm is proposed in (Olaru *et al.*, 2004) and in (Thomas *et al.*, 2005). Explicit-MPC is proposed in (Bemporad *et al.*, 2000a and 2000b) where the optimization problem is treated as a multi-parametric problem solved off-line; and hence on-line computation reduces to a function evaluation. However, all these techniques have been developed for linear hybrid systems.

An Analytical Nonlinear Model Predictive Control (ANMPC) technique for linear induction motor is proposed in (Thomas and Hansson, 2010 and 2013), and ANMPC for nonlinear hybrid systems with discrete inputs only is presented in (Thomas, 2012). The proposed ANMPC controller based on enumerating all possible inputs combination and calculating analytically the cost function and then selects the input combination which minimizes the cost function. The author of (Thomas, 2012) shows that ANMPC lead to MPC with lower computation load compared to other techniques proposed in literature i.e. standard B&B, explicit MPC for the considered classes of hybrid systems with discrete inputs only, and that ANMPC an take into account state and output constraints.

This paper propose extending the ANMPC controller by integrating it with Particle Swarm Optimization (PSO) (Kennedy and Eberhart, 1995) and show that the new proposed controller can be applied effectively to nonlinear hybrid systems with discrete and continuous inputs. This algorithm reduces efficiently the computation load while respecting the given input, states and output constraints. Besides, the new proposed technique can control directly nonlinear hybrid systems avoiding linearization which may lead to inaccurate model and unexpected behaviour.

The rest of the paper is organized as following; section 2 briefly presents the concepts of MPC and

PSO. The proposed ANMPC integrated with PSO controller is developed in section 3. Application of the proposed controller to a three-tanks example is considered in section 4. Finally conclusion and some remarks are given in section 5.

2 CONCEPTS OF MPC AND PSO CONTROLLERS

2.1 Model Predictive Control

Predictive control was first developed at the end of 1970s, and was published by Richalet *et al.*, (1978). In the 1980s, many methods based on the same concepts are developed. Those types of controls are now grouped under the name Model Predictive Control (MPC) (Camacho and Bordons, 1999). MPC has proved to efficiently control a wide range of applications in various industries.

The main idea of predictive control is to use a model of the plant to predict future outputs of the system. Based on this prediction, at each sampling period, a sequence of future control values is developed through an on-line optimization process, which maximizes the tracking performance while satisfying constraints. Only the first value of this optimal sequence is applied to the plant. The whole procedure is repeated again at the next sampling period according to the ‘receding’ horizon strategy (Maciejowski, 2002). The objective is to lessen the future output error to zero with minimum input effort. The cost function to be minimized is generally a weighted sum of square predicted errors and square future control values, e.g., in Generalized Predictive Control (Clarke *et al.*, 1987):

$$J(N, N_u) = \sum_{j=1}^N \beta [\hat{y}(k+j|k) - w(k+j)]^2 + \sum_{j=1}^{N_u} \lambda [u(k+j-1)]^2 \quad (1)$$

where \hat{y}, u are the predicted output and the control signal respectively. N, N_u are the prediction horizons and the control horizon, respectively. β, λ are weighting factors. The control horizon permits a decrease in the number of the calculated future control assuming $\Delta u(k+j) = 0$ for $j \geq N_u$. $w(k+j)$ is the reference trajectory.

Constraints over the control signal, the outputs and the control signal changing, can be added to the cost function:

$$\begin{aligned} u_{\min} &\leq u(k) \leq u_{\max} \\ \Delta u_{\min} &\leq \Delta u(k) \leq \Delta u_{\max} \\ y_{\min} &\leq y(k) \leq y_{\max} \end{aligned} \quad (2)$$

The solution of (1) gives the optimal sequence of the control signal over the horizon N_u while respecting the given constraints of (2).

A fundamental difficulty of the MPC approach is the requirement to solve constrained nonlinear, nonconvex optimization problems. A linearized model of nonlinear systems is commonly used for MPC controller. However, this linearization introduces model mismatches which affect the control performance, as the MPC performance depends largely on the accuracy of the process’ model.

2.2 Particle Swarm Optimization

The particle swarm optimization (PSO) algorithm is a population-based search algorithm inspired by the social behavior of birds within a flock (Kennedy and Eberhart, 1995). Particle Swarm has two primary operators: Position and Velocity. Each particle representing a potential solution is maintained within a swarm. The position of each particle is adjusted according to the experience of itself and its neighbours. During each generation, each particle is accelerated toward the particle’s previous best position p , and the global best position g . At each iteration, a new velocity value for each particle is calculated based on its current velocity, the distance from its previous best position, and the distance from the global best position. The new velocity value is then used to calculate the next position of the particle in the search space. This process is then reiterated a set number of times, or until a minimum error is achieved. The PSO with Constriction Coefficient is considered where velocity and position are updated according to the following equations (Clerc and Kennedy, 2002):

$$v_{ij}(t) = \chi [v_{ij}(t-1) + c_1 r_1 (p_{ij} - x_{ij}(t-1)) + \dots + c_2 r_2 (g_j - x_{ij}(t-1))] \quad (3)$$

$$x_{ij}(t) = x_{ij}(t-1) + v_{ij}(t) \quad (4)$$

where $x_{ij}(t)$, $v_{ij}(t)$ and p_{ij} are the position, velocity and best personal position of particle i , in dimension $j = 1, 2, \dots, n_x$ at iteration t , where n_x is the dimension of the system inputs. g_j is the global best position in dimension j . c_1 and c_2 are

constants, and r_1, r_2 are random values in the range $[0;1]$. χ is the constriction coefficient.

PSO has been found to be robust in solving continuous nonlinear optimization problems as well as capable of generating high quality solutions with more stable and faster convergence characteristics, and shorter calculation times than other stochastic methods. It has been shown in the literature that PSO can efficiently control wide range of systems especially those with continuous control signals, see for example (Sedighzadeh and Masehian, 2009), (Poli, 2008) and references therein.

3 INTEGRATING PSO WITH ANMPC FOR NONLINEAR HYBRID SYSTEMS

The main ideas of the proposed controller; integrating Particle Swarm Optimization with the Analytical Nonlinear Model Predictive Control (PSO-ANMPC), for nonlinear hybrid systems are:

- Using the PSO algorithm, find iteratively the optimal/sub-optimal solution for the continuous control signals that minimize the fitness function.
- For each solution (particle) of the continuous control signals, find the best combination of the discrete control signals using the ANMPC.
- The fitness function of the PSO is the optimization cost function of the MPC controller.

Each particle's position in the swarm integrated with its best combination of discrete inputs, together, represents a solution to the NMPC optimization problem. i.e., the inclusion of the control sequence over the control horizon. Thus, each particle dimension is $n_c \times N_u$, and the dimension of the optimization vector of the ANMPC is $n_d \times N_u$, where n_c, n_d are the number of continuous input variables and discrete input variables respectively. The effectiveness of each solution is calculated through the fitness function, which in this case is the considered cost function of the NMPC controller. However, it is important to mention here that PSO is a gradient-free technique, thus any cost function that represents the desired behavior can be chosen. The proposed technique avoids any linearization technique for minimization, albeit at an increased computational complexity.

The global best PSO is considered where each particle is connected to and able to obtain information from every other particle in the swarm.

(Bratton and Kennedy, 2007). Global best PSO exhibits very fast convergence rates which are much needed for predictive control application.

Considering the discrete input variables, there are limited or finite numbers of possible input combinations for the discrete input variables i.e. $\mathbf{u}^d(k) \in \chi_u^d$, where χ_u^d is the set of possible discrete input combinations. Thus the optimal control signal for these variables will be one combination of the possible input combinations.

The PSO-ANMPC can be implemented through the following Algorithm:

Algorithm 1

- 1- Let p^k is a particle in the swarm for $k=1,2,\dots,N_d$, where N_d is number of particles in the population.
 $p^k =: \mathbf{u}^{ck} = [\mathbf{u}^c(k), \mathbf{u}^c(k+1), \dots, \mathbf{u}^c(k+N-1)]$
 and let:
 $\mathbf{u}^{di} = [\mathbf{u}^d(k), \mathbf{u}^d(k+1), \dots, \mathbf{u}^d(k+N-1)] \in \chi_u^d$
 is the i -th possible discrete control sequence over horizon N
- 2- Initializing the particles position and velocity of the PSO, and let $J_{opt} = \infty$
- 3- For $j=1:N_t$ (N_t max. number of iterations)
- 4- For each p^k
- 5- while χ_u^d is non empty, where χ_u^d is the set of possible input combinations over horizon N
- 6- Select $\mathbf{u}^i \in \chi_u^d$, and remove it from the set χ_u^d
- 7- Compute J^i the cost function according to the control combination \mathbf{u}^i , where: $\mathbf{u}^i = [\mathbf{u}^c \quad \mathbf{u}^d]^T$.
- 8- If $J^i < J_{opt}$
 $J_{opt} = J^i$, and $\mathbf{u}^* = \mathbf{u}^i$,
 End
 end
 End
- 9- update the particles position and velocity
 End
- 10- $\mathbf{u}_{opt}^* = \mathbf{u}^i$ the optimal control signal

This technique which we call it PSO-ANMPC has many advantages. It reduces the computation time significantly; because from one hand: computing analytically the cost function is faster than building

or reformulating the problem as MIQP or MILP problem and then solving it, and from the other hand the proposed analytical NMPC has often less number of possible input combination than formulating it classically in a hybrid system framework, e.g. MLD systems (Bemborad and Morari, 1999); to explain that in a simple way, consider a system with one discrete input variable which may have a value among m possible discrete values, this will be modeled in the MLD form by m binary variables which leads to a number of possible input combinations over control horizon N equal $2^{m \times N}$, while the number of possible input combinations with the proposed PSO-ANMPC controller for the same system will equal m^N only.

One of the main advantages of the proposed controller is its ability to deal directly with nonlinear hybrid systems, where modeling and controlling of nonlinear hybrid systems is normally a hard task and it is very common to linearize the model, but this linearization could lead to a complex system with many different linear models around different operating points and/or could introduces uncertainty which may lead to inaccurate model affecting the efficiency of designed or used controller. The advantage of the technique presented here is that we do not need to linearize the system, and non-linear dynamics can be directly used to calculate the new states and outputs. Moreover, The proposed controller is easy to construct, to tune and to implement.

3.1 Reduction Algorithm

To avoid examining all possible discrete input combinations over the control horizon N the following Algorithm is proposed.

Algorithm 2

- 1- Initializing with $J_{opt} = \infty, J^i(k) = 0$
- 2- For $\mathbf{u}^i, i \in \{1, 2, \dots, s\}$ where s is the total number of possible input combinations over horizon N
- 3- For $j = 1 : N$
 - 4- Compute $J^i(k+j)$ the cost function according to the control combination \mathbf{u}^i for horizon j as follows:
$$J^i(k+j) = J^i(k+j-1) + f(\mathbf{x}(k+j), \mathbf{u}^i(k+j-1))$$
 where $f(\mathbf{x}(k+j), \mathbf{u}^i(k+j-1))$ is the cost

at instant $(k+j)$ due to the control signal $\mathbf{u}^i(k+j-1)$.

- 5- If $J^i(k+j) > J_{opt}$
 - Break and go to step 2
 - end
- end
- 6- At $j = N$
 - If $J^i(k+N) < J_{opt} \rightarrow J_{opt} = J^i(k+N)$
 - end
- End
- 7- $J^*_{opt} = J_{opt}$ the optimal solution

Algorithm 2 stops the cost function calculations at prediction step $(k+j)$ where $1 < j < N$ for the control sequence \mathbf{u}^i over the horizon N if the cost function at this prediction step is higher than the current upper boundary J_{opt} .

Algorithm 2 could also be used as suboptimal solution if the computation time is higher than the sampling time, the Algorithm could stop at any instant and send the control signals according to the current J_{opt} as a suboptimal solution.

3.2 Constraints

In this section, we describe how system constraints can be included in the optimization problem so that PSO-ANMPC can offer a suboptimal solution while respecting the given constraints.

3.2.1 Input Constraints

Constraints over the control signal $u_{j \min}^c \leq u_j^c(k) \leq u_{j \max}^c$ can be implemented by limiting the search space in the PSO algorithm: $x_{ij}(t) \in [x_{j \min}, x_{j \max}]$, where $x_{j \min}, x_{j \max}$ are the control signal constraints $u_{j \min}^c, u_{j \max}^c$, respectively, given that the discrete control signals are limited by their discrete values.

Constraints over the control signal variation $|\Delta u_j(k)| \leq \Delta u_{j \max}$ can be represented through the particles velocity limits, as follows:

$$v_{ij}(t) = \begin{cases} v_{ij}(t) & \text{if } v_{ij}(t) \leq V_{j \max} \\ V_{j \max} & \text{if } v_{ij}(t) > V_{j \max} \end{cases} \quad (5)$$

where $V_{j_{\max}}$ is the maximum allowable control variation for the control element j .

3.2.2 Output and System States Constraints

Output signals and system states can be subject to hard and/or soft constraints. Hard constraints could, for example, relate to safety or physical constraints, while soft constraints may be related to economic constraints or better working conditions.

Both of hard and soft constraints can be included in the proposed controller. Hard constraints on output and state variables can be simply considered by adding the following line to Algorithm 2:

$$\text{if } x(y) > x_{\max}(y_{\max}) \rightarrow J^i(k+j) = \infty \quad (6)$$

Thus any control combination which will lead to violation of the output or state hard constraints will be avoided.

Soft constraints which allow, at a price, temporary violation of some constraints, can also be included as following:

$$y(x) \leq y_{\max}(x_{\max}) + \varepsilon \quad (7)$$

Adding the following term to the cost function:

$$J^i(k+j) = \dots + \varepsilon(k+j)^T Q \varepsilon(k+j) \quad (8)$$

where Q are positive definite weighting matrix. This additional term in Equation (8) penalize the violation of soft constraints, pushing the system to have $\varepsilon = \text{zeros}$. Effectively, we are saying that the constraints are allowed to be violated to a degree, but doing so costs, and should thus be avoided if possible.

4 APPLICATION

The proposed control strategy is applied on the three tanks example. The simplified physical description of the three tanks system is presented in Figure 1 (see Dolanc *et al.*, 1997, for more details).

The system consists of three tanks, filled with water by two independent pumps acting on tanks 1 and 2. These two pumps are continuously manipulated from 0 up to a maximum flow Q_1 and Q_2 respectively. Four switching valves V_1 , V_2 , V_{13} and V_{23} control the flow between the tanks, those valves are assumed to be either completely opened or closed ($V_i = 1$ or 0 respectively). The V_{N3} manual valve controls the nominal outflow of the

middle tank. It will be assumed in further simulations that the V_{L1} and V_{L2} valves are always closed and V_{N3} is open. The liquid levels to be controlled are denoted h_1 , h_2 and h_3 for each tank respectively.

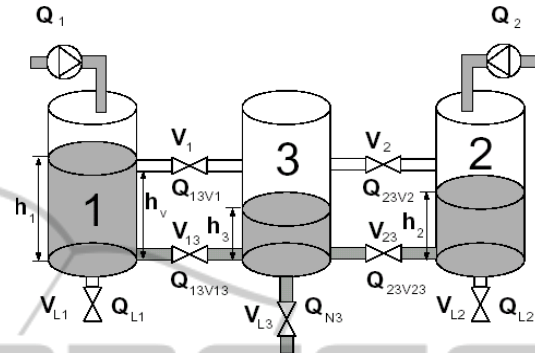


Figure 1: COSY three tank benchmark system.

The conservation of mass in the tanks provides the following differential equations:

$$\begin{aligned} \dot{h}_1 &= \frac{1}{A} (Q_1 - Q_{13V1} - Q_{13V13}) \\ \dot{h}_2 &= \frac{1}{A} (Q_2 - Q_{23V2} - Q_{23V23}) \\ \dot{h}_3 &= \frac{1}{A} (Q_{13V1} + Q_{13V13} + Q_{23V2} + \\ &\quad + Q_{23V23} - Q_N) \end{aligned} \quad (9)$$

where the Q 's denote the flows and A is the cross-sectional area of each of the tanks. The Toricelli's law provides the expressions of the flows through the valves, which are given by the relations:

$$\begin{aligned} Q_{i3V13} &\approx k_{i3} V_{i3} (h_i - h_3) \\ Q_{i3Vi} &\approx k_i V_i (\max(h_v, h_i) - \max(h_v, h_3)) \\ Q_{N3} &\approx k_{N3} V_{N3} h_3 \end{aligned} \quad (10)$$

$$\text{where: } k_{i3} = a_z S_{i3} \sqrt{\frac{2g}{h_{\max}}}, \quad i=1,2$$

$$k_i = a_z S_i \sqrt{\frac{2g}{h_{\max} - h_v}} \quad k_{N3} = a_z S_{N3} \sqrt{\frac{2g}{h_{\max}}}$$

From these expressions, a model is derived with the following variables:

$$\begin{aligned} \mathbf{x} &= [h_1 \quad h_2 \quad h_3]' \\ \mathbf{u} &= [Q_1 \quad Q_2 \quad V_1 \quad V_2 \quad V_{13} \quad V_{23}]' \end{aligned} \quad (11)$$

The following specifications are considered: starting from zero levels (the three tanks being

empty), the objective of the control strategy is to reach the liquid levels $h_1 = 0.5 \text{ m}$, $h_2 = 0.5 \text{ m}$ and $h_3 = 0.1 \text{ m}$.

As presented in (Thomas *et al.*, 2006), studying the dynamic behavior of the three tanks, starting from zero levels to the desired ones, enables to divide the state space into three main regions, each one with its adequate simple MLD model; for example in the sub-region where the liquid level in the three tanks are less than the valves level, it clearly appears that the two valves V_1 and V_2 of the input vector are not in progress, thus $\mathbf{u} = [Q_1 \ Q_2 \ V_{13} \ V_{23}]'$.

Obviously the particles of PSO will consider the continuous signals (the two pumps), while ANMPC will investigate the best position combination of the four valves. The proposed PSO-ANMPC has been implemented in simulation to reach the level specification with the following parameters: The parameters of the PSOMPC controller that give a good response are: $c_1 = c_2 = 2.05$, $\chi = 0.73$, with 10 particles per swarm and a maximum number of iterations 10. A control horizon $N = N_u = 2$ is chosen. Weights in the objective function (1) have been chosen as $\beta = \text{diag.}(10000, 1000, 100000)$ and $\lambda = 1$. Search space and velocity limits are chose according to the pumps limits as follows:

$$[x_i] \in \left[\begin{array}{c} 0 \\ 0 \end{array}, \begin{array}{c} Q_{\max} \\ Q_{\max} \end{array} \right], \quad v_{i \min} = \begin{bmatrix} -Q_{\max} \\ -Q_{\max} \end{bmatrix},$$

$$v_{i \max} = \begin{bmatrix} Q_{\max} \\ Q_{\max} \end{bmatrix}, \quad \text{where } Q_{\max} = 0.0001$$

The global best PSO is used for the PSO with a constriction coefficient. The solution at instant $k - 1$ is memorized and introduced as a particle in the initial population at instant k . The results are presented on Figure 2 for the tanks levels and on Figure 3 for the control signals. The level of the third tank oscillates around 0.1 as $h_3 = 0.1$ does not correspond to an equilibrium point. Consequently, the system opens and closes the two valves V_1 and V_2 to maintain the level in the third tank around the desired level of 0.1m. The system has been simulated in Matlab envirement.

The computation times per step is in order of *ms*. i.e. is much smaller than the sampling time (the sampling time of the three tanks benchmark is 10 s.). Thus real-time application is possible even for

longer horizon. The PSO-ANMPC technique reduces the computation time and provides opportunities for real-time implementation; avoiding exponential explosion of the algorithm.

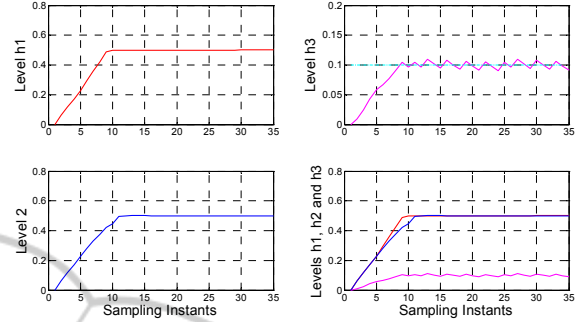


Figure 2: Water levels in the three tanks.

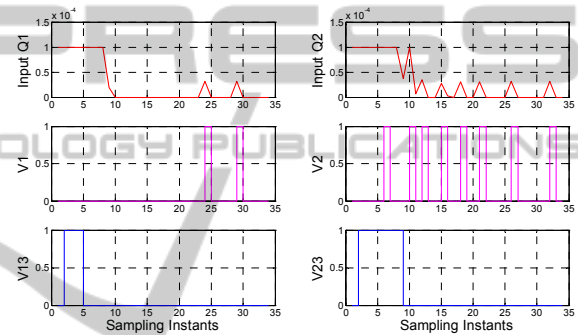


Figure 3: Controlled variables.

Figures 4 and 5 respectively present the three tanks levels and the control signals with PSO-ANMPC technique, where the desired level in the third tank is changing. It can be seen that the proposed controller can successfully tracking the desired levels. It must be noticed that the variation of the third tank level from 0.15 to 0.1 takes more time than the variation from 0.1 to 0.15, due to the benchmark physical features.

Increasing the number of particles per swarm and the maximum number of iteration will improve

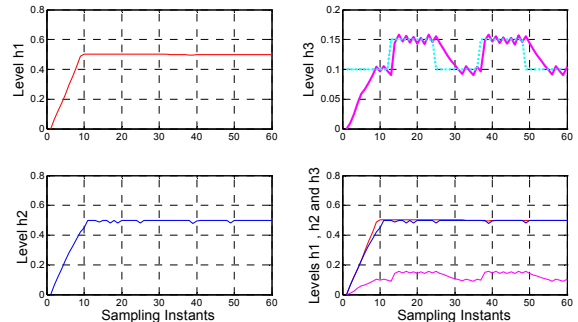
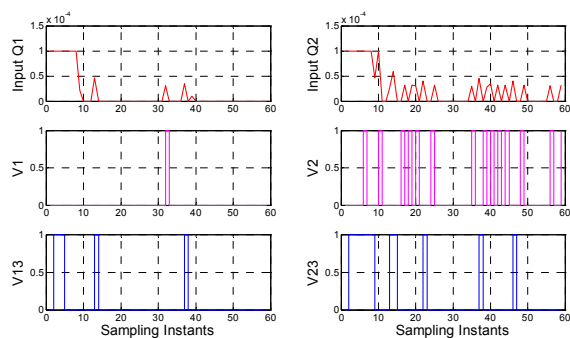


Figure 4: Water levels in the three tanks – h_3 changes.


 Figure 5: Controlled variables – h_3 changes.

the suboptimal solution, and increases the opportunities to find the optimal solution; however this will increase the computation time. The selection of the number of particles and the maximum number of iteration is a trade-off, and is based on the dynamics of the process to be controlled.

5 CONCLUSIONS

This paper presented integrating Particle Swarm Optimization with Analytical Nonlinear Model Predictive Control (PSO-ANMPC) for constrained nonlinear hybrid systems with discrete and continuous control signals. The proposed PSO-ANMPC controller offers a suboptimal solution in reasonable time, thus increases the opportunities of real-time application for many nonlinear hybrid systems. It can be applied directly to nonlinear hybrid systems, thus no need to linearize the nonlinear dynamics as usually done with other techniques. PSO-ANMPC can be applied to some classes of hybrid systems including constrained nonlinear systems, constrained non-convex optimization problems and fast dynamic hybrid systems. The proposed controller has the ability to consider hard and soft constraints. However, there is no guarantee to find the optimal solution.

An application of the PSO-ANMPC controller to a three-tanks example showed that it reduces significantly the computational time, which is an inherent drawback of classical MPC controllers. Therefore, real-time implementation of the proposed PSO-ANMPC controller is possible.

Future work will include experimental works to validate this technique in practice, as well as, improving the algorithm and applying it to other classes of hybrid systems.

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